



**(43) International Publication Date**  
**27 May 2004 (27.05.2004)**

**PCT**

**(10) International Publication Number**  
**WO 2004/044848 A1**

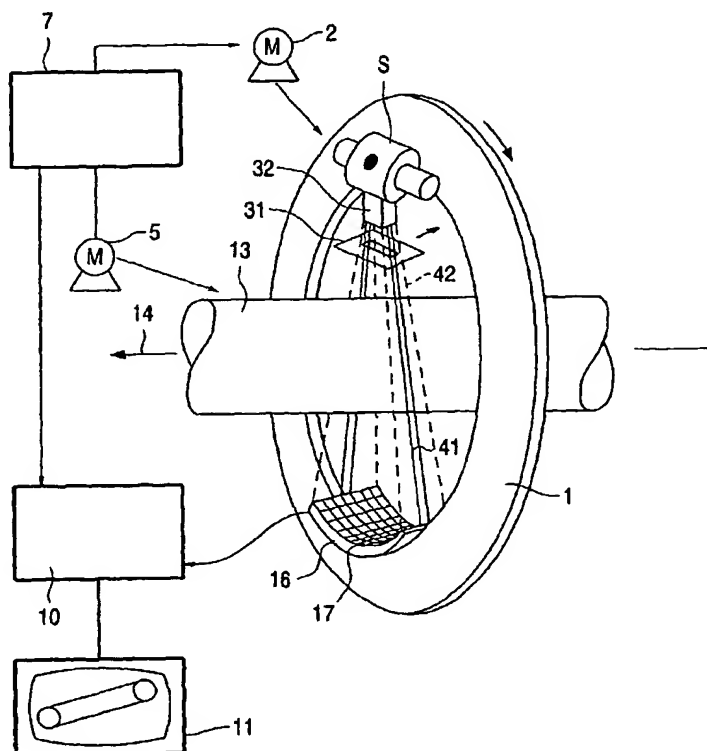
- (51) International Patent Classification<sup>7</sup>:** **G06T 11/00,**  
A61B 6/03
- (21) International Application Number:**  
PCT/TB2003/004749
- (22) International Filing Date:** 24 October 2003 (24.10.2003)
- (25) Filing Language:** English
- (26) Publication Language:** English
- (30) Priority Data:**  
102 52 662.1 11 November 2002 (11.11.2002) DE
- (71) Applicant (for DE only):** **PHILIPS INTELLECTUAL PROPERTY & STANDARDS GMBH [DE/DE];** Stein-  
damm 94, 20099 Hamburg (DE).
- (71) Applicant (for AE, AG, AL, AM, AT, AU, AZ, BA, BB, BE, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU, CY, CZ, DK, DM, DZ, EC, EE, EG, ES, FI, FR, GB, GD, GE, GH, GM, GR, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX,**

**MZ, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RU, SC, SD, SE, SG, SK, SL, SY, SZ, TJ, TM, TN, TR, TT, TZ, UA, UG, UZ, VC, VN, YU, ZA, ZM, ZW only): KONINKLIJKE PHILIPS ELECTRONICS N.V. [NL/NL]; Groenewoudseweg 1, NL-5621 BA Eindhoven (NL).**

- (72) **Inventors; and**  
(75) **Inventors/Applicants (for US only): SCHLOMKA, Jens-Peter** [DE/DE]; c/o Philips Intellectual Property & Standards GmbH, Weissshausstr. 2, 52066 Aachen (DE).  
**GRAB, Michael** [DE/DE]; c/o Philips Intellectual Property & Standards GmbH, Weissshausstr. 2, 52066 Aachen (DE).  
(74) **Agent: VOLMER, Georg**; Philips Intellectual Property & Standards GmbH, Weissshausstr. 2, 52066 Aachen (DE).  
(81) **Designated States (national):** AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK,

*[Continued on next page]*

- (54) Title: COMPUTED TOMOGRAPHY AND METHOD WITH THREE-DIMENSIONAL BACKPROJECTION



**(57) Abstract:** The invention relates to a computed tomography method in which an examination zone is irradiated along a circular trajectory by a fan-shaped radiation beam. Radiation coherently scattered in the examination zone is measured by a detector unit, the variation in space of the scatter intensity in the examination zone being reconstructed from said measuring values. Reconstruction is performed by back projection in a volume which is defined by two linearly independent vectors of the rotational plane and a wave vector transfer.



MN, MW, MX, MZ, NI, NO, NZ, OM, PG, PH, PL, PT,  
RO, RU, SC, SD, SE, SG, SK, SL, SY, TJ, TM, TN, TR,  
TT, TZ, UA, UG, US, UZ, VC, VN, YU, ZA, ZM, ZW.

SE, SI, SK, TR), OAPI patent (BF, BJ, CF, CG, CI, CM,  
GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

(84) **Designated States (regional):** ARIPO patent (GH, GM,  
KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZM, ZW),  
Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM),  
European patent (AT, BE, BG, CH, CY, CZ, DE, DK, EE,  
ES, FI, FR, GB, GR, HU, IE, IT, LU, MC, NL, PT, RO,

**Published:**

— with international search report

*For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.*

COMPUTED TOMOGRAPHY DEVICE AND METHOD WITH THREE-DIMENSIONAL BACKPROJECTION

The invention relates to a computed tomography method in which an examination zone is irradiated along a circular trajectory by a fan-shaped radiation beam and in which a detector unit detects primary radiation and radiation which is coherently scattered in the examination zone. The invention also relates to a computer tomograph for carrying out  
5 such a method as well as to a computer program for controlling the computer tomograph.

In known methods of the kind set forth radiation which is coherently scattered in the examination zone is measured by a detector unit; the variation in space of the scatter  
10 intensity in the examination zone is then reconstructed from said measuring values. The reconstruction is usually carried out by means of iterative methods based on algebraic reconstruction techniques (ART) in which a reconstruction of the entire irradiated examination zone is necessary. A reconstruction of a part of the examination zone is not possible. Moreover, the iterative methods require a large amount of calculation work and  
15 hence lead to comparatively long reconstruction times. Alternative methods involve two-dimensional reconstruction techniques based on back projection; in these techniques such large distances exist or are assumed between the examination zone and the detector unit that an unambiguous relationship exists between the point of incidence of a scattered ray on the detector unit and the scatter angle. However, this geometry cannot be realized in medical  
20 applications, so that the two-dimensional back projection produces inaccurate results only.

Therefore, it is an object of the present invention to provide a method, a computer tomograph as well as a computer program which enable a faster reconstruction of  
25 the scatter intensity distribution in the examination zone while taking into account the actual geometry in medical applications.

In respect of the method this object is achieved in accordance with the invention by means of a computed tomography method which comprises the steps of

- generating, using a radiation source and a diaphragm arrangement which is arranged between the examination zone and the radiation source, a fan beam which traverses an examination zone or an object present therein,
- generating relative motions, comprising a rotation about an axis of rotation, between  
5 the radiation source on the one side and the examination zone or the object on the other side,
- acquiring measuring values which are dependent on the intensity of the radiation by means of a detector unit which detects, during the relative motions, the primary radiation from the fan beam and radiation which is coherently scattered in the  
10 examination zone or on the object,
- reconstructing a CT image of the examination zone from the measuring values, during which reconstruction a back projection is carried out in a volume which is defined by two linearly independent vectors of the rotational plane and a wave vector transfer.

The scatter intensity is dependent not only on the material but also on the  
15 scatter angle and the wavelength of the radiation. A back projection in a volume defined by two linearly independent vectors of the rotational plane and a wave vector transfer, however, has the advantage that the scatter intensity thus parameterized is dependent exclusively on the scatter material, because the wave vector transfer is known to be proportional to the product of the inverse wavelength and the sine of half the scatter angle. In this context the scatter  
20 angle is the angle which is enclosed by the path of the scattered ray relative to the path that the ray would have followed in the absence of the scattering process.

The scattered rays have a curved shape in said volume. Taking the curved shape of the scattered rays into account for the back projection in conformity with claim 2 enhances the quality of the reconstructed scatter intensity distribution.

25 According to the preferred reconstruction method disclosed in claim 3 the measuring values are weighted prior to the back projection. Such weighting takes into account the fact that the effectiveness of the detector surface decreases as the scatter angle increases and also that the radiation density decreases as the distance between the point of incidence of the scattered ray on the detector unit and the scatter center increases. The  
30 effective detector surface is the detector surface projected in a plane perpendicular to the path of the detected ray. The weighting in claim 4 takes into account the fact that the radiation density decreases as the distance between the radiation source and the scatter center increases. The quality of the reconstructed scatter intensity distribution is enhanced when such effects are taken into account.

Claim 5 describes a preferred reconstruction method which requires less calculation work in comparison with other methods and offers a favorable image quality nevertheless.

5 A computer tomograph for carrying out the method in accordance with the invention is disclosed in claim 6.

Claim 7 defines a computer program for controlling a computer tomograph as disclosed in claim 6.

10 The invention will be described in detail hereinafter on the basis of an embodiment and with reference to a drawing; therein:

Fig. 1 shows a computer tomograph which is suitable for carrying out the method in accordance with the invention,

15 Fig. 2 is a diagrammatic cross-sectional view of the computer tomograph of Fig. 1 in the direction of the axis of rotation,

Fig. 3 shows a flow chart of a version of the method in accordance with the invention,

Fig. 4 is a plan view of a column of detector elements,

20 Fig. 5 is a diagrammatic representation of the arrangement of virtual radiation source,

Fig. 6 shows a cross-section through the rays of the virtual radiation sources,

Fig. 7 is a diagrammatic sectional view of the irradiated examination zone and the detector in the direction of the plane of rotation, and

25 Fig. 8 illustrates the dependence of the amount of the wave vector transfer on the distance between a scatter center in the examination zone and the foot of the detector (point of incidence of the primary beam on the detector unit).

30 The computer tomograph shown in Fig. 1 comprises a gantry 1 which is capable of rotation about an axis of rotation 14. To this end, the gantry 1 is driven by a motor 2 at a preferably constant, but adjustable angular speed. A radiation source S, for example, an X-ray source, is mounted on the gantry 1. A diaphragm arrangement 31 defines a radiation fan beam 41 which is used for the examination and is denoted by solid lines in Fig. 1. The fan beam 41 extends perpendicularly to the axis of rotation 14 and has small dimensions in the

direction thereof, for example, 1 mm. Between the diaphragm arrangement 31 and the radiation source S there may be arranged a second diaphragm device 32 which forms a conical radiation beam 42 from the radiation generated by the X-ray source S. The conical radiation beam 42, which would arise in the absence of the diaphragm arrangement 31, is denoted by dashed lines.

The fan beam 41 traverses a cylindrical examination zone 13 in which an object, for example, a patient on a patient table (both not shown) or also a technical object may be situated. After having traversed the examination zone 13, the fan beam 41 is incident on a detector unit 16 which is attached to the gantry 1 and comprises a measuring surface 17 with a plurality of detector elements arranged in the form of a matrix. The detector elements are arranged in rows and columns. The detector columns extend parallel to the axis of rotation 14. The detector rows are situated in planes which extend perpendicularly to the axis of rotation, that is, preferably on an arc of a circle around the radiation source S. However, they may also have a different shape, for example, the shape of an arc of a circle around the axis of rotation, or be rectilinear. Generally speaking, the detector rows comprise substantially more detector elements (for example, 1000) than the detector columns (for example, 16).

The fan beam 41, the examination zone 13 and the detector unit 16 are adapted to one another. In a plane perpendicular to the axis of rotation 14 the dimensions of the fan beam 41 are chosen to be such that the examination zone 13 is fully irradiated and the length of the rows of the detector unit 16 is such that the fan beam 41 can be detected completely. The fan beam is incident on the central detector row (rows).

When a technical object is concerned instead of a patient, the object can be rotated during an examination while the radiation source S and the detector unit 16 remain stationary. The examination zone 13, or the object or the patient table, can be displaced parallel to the axis of rotation 14 by means of a motor 5. As an equivalent, however, the gantry could also be displaced in this direction.

When the motors 2 and 5 operate simultaneously, the radiation source S and the detector unit 16 describe a helical trajectory relative to the examination zone 13. However, when the motor 5 for the displacement in the direction of the axis of rotation 14 is stationary and the motor 2 rotates the gantry, a circular trajectory is obtained for the radiation source S and the detector 16 relative to the examination zone 13. Hereinafter only the circular trajectory will be considered.

Fig. 2 shows that between the examination zone 13 and the detector unit 16 there is arranged a collimator arrangement 6 which comprises a plurality of blades 60. The blades 60 consist of a material which strongly absorbs the X-rays and are situated in planes which extend parallel to the axis of rotation 14 and intersect one another at the focus of the radiation source S. Their spacing may amount to, for example, 1 cm and each blade 60 may have a dimension of, for example, 20 cm in the plane of drawing. The collimator arrangement 6 thus subdivides the fan beam 41 into a number of neighboring segments, so that essentially a column of detector elements is struck by primary or scattered radiation from one segment only.

The measuring values acquired by the detector unit 16 are applied to an image processing computer 10 which is connected to the detector unit 16, for example, via a wireless data transmission. The image processing computer 10 reconstructs the scatter intensity distribution in the examination zone 13 and reproduces it, for example, on a monitor 11. The two motors 2 and 5, the image processing computer 10, the radiation source S and the transfer of the measuring values from the detector unit 16 to the image processing computer 10 are controlled by a control unit 7.

In other embodiments the acquired measuring values can first be applied to one or more reconstruction computers for reconstruction, which reconstruction computers apply the reconstructed data to the image processing computer, for example, via an optical fiber cable.

Fig. 3 shows a flow chart illustrating the execution of a version of a measuring and reconstruction method that can be carried out by means of the computer tomograph shown in Fig. 1.

After the initialization in the step 101, the gantry rotates at a constant angular speed. In the step 103 the radiation of the radiation source S is switched on so that the detector unit 16 can detect the primary and the scattered radiation from a plurality of angular positions. The detector element or elements at the center of each detector column detect essentially the primary radiation, whereas the scattered radiation (secondary radiation) is detected by the detector elements which are situated further nearer to the ends of a column.

The foregoing is diagrammatically indicated in Fig. 4 which is a plan view of a column of detector elements. The detector elements 161 which detect the scattered radiation are denoted by simple shading whereas the detector element 160 which is situated at the center and detects the primary radiation is marked by a cross. In other radiation sources, notably in radiation sources having a larger focus, the primary radiation could also be

detected by more than one detector element. To both sides of the central detector element there are situated detector elements which are struck by scattered radiation, but also by a (reduced) amount of primary radiation (white elements neighboring 160) because of the finite dimensions of the focus of the radiation source. In this embodiment scattered radiation is considered to be only the radiation which is measured by the detector elements denoted by shading in the drawing.

The scatter intensity is dependent inter alia on the energy of the scattered X-ray quantum. Therefore, the energy of the scattered X-ray quantum must either be measured, implying that the detector elements should be capable of measuring in an energy-resolved fashion, or use must be made of X-rays with quantum energies from an as small as possible range (monochromatic X-rays in the ideal case). There are various possibilities for minimizing the energy difference of the X-ray quanta relative to their energy:

- The use of suitable filter materials, for example, copper in the primary beam. As a result, the soft X-rays generated by an X-ray source, that is, X-rays having a low quantum energy, are suppressed to a high degree.
- Additionally, the voltage of an X-ray tube can be optimized with respect to the selected filter.
- Finally, the so-called "balanced filter" technique can be applied. According to this technique the data is acquired twice and each time filters which have a slightly different atomic number and whose K edge is used for filtering are then situated in the beam path. Subsequently, the difference signal from the two measurements is extracted.

In the step 105 the measuring values of the scattered radiation are normalized. The measuring values of each radiation source position of the scattered radiation are then divided by the measuring values of those primary rays which have caused the scattered rays.

In the step 107 the measuring values are subjected to a rebinning operation. Each measuring value is then associated with a line from the detector element in which the measuring value has been detected to the radiation source position. Thus, it is assumed that rays of the fictitious, conical radiation beam 42 have caused the measuring values without the rays having been scattered. Due to the rebinning operation the measuring values are resorted as if they had been measured by means of a different radiation source (a circular radiation source capable of emitting mutually parallel fan beams) and a different detector (a flat, rectangular virtual detector).



This will be described in detail with reference to Fig. 5. Therein, the reference numeral 17 denotes the circular trajectory along which the radiation source irradiates the examination zone. The reference numeral 413 denotes a fan-shaped radiation beam which emanates from the radiation source position  $S_0$  and whose rays propagate in a plane containing the axis of rotation 14. The conical radiation beam emitted by the radiation source in the position  $S_0$  may be assumed to consist of a plurality of flat fan beams which are situated in planes which are parallel to the axis of rotation 14 which intersect in the radiation source position. Fig. 5 shows only a single one of these fan beams, that is, the fan beam 413.

Moreover, Fig. 5 also shows further fan beams 411, 412 and 414, 415 which extend parallel to the fan beam 413 and are situated in planes which are parallel to one another and to the axis of rotation 14. The associated radiation source positions  $S_{-2}$ ,  $S_{-1}$  and  $S_1$ ,  $S_2$  are occupied by the radiation source S before and after reaching the radiation source position  $S_0$ , respectively. All rays in the fan beams 411 to 415 have the same projection angle. The projection angle is the angle enclosed by the planes of the fan beams with respect to a reference plane which is parallel to the axis of rotation 14.

The fan beams 411 to 415 define a radiation beam 410 having a tent-like shape. Figs. 5 and 6 show the sectional area 420 which is obtained when the radiation beam 410 is intersected by a plane which contains the axis of rotation 14 and extends perpendicularly to the planes of the fan beams 411 to 415. The two edges of the sectional area 420 which intersect the axis of rotation are curved. This curvature is due to the fact that the radiation source position at the center (for example,  $S_0$ ) are situated further from the sectional plane than those at the edge (for example,  $S_2$  or  $S_{-2}$ ) and that the fan beams all have the same angle of aperture. For each group of fan beams, therefore, a rectangular virtual detector 170 is defined in the plane sectional area 420, the edges 171 and 172 of said virtual detector being given by the dimensions of the outer fan beams 411 and 415 in the plane sectional area.

Fig. 6 also shows (marked by round dots) the puncture points of some rays, contained in the fan beams 411 ... 415, through said virtual detector. Finally, crosses mark the supporting points of a regular cartesian grid. The puncture points and the supporting points usually do not coincide. From the measuring values for the puncture points, therefore, the measuring values at the equidistant supporting points within the virtual detector 170 have to be determined. Such rebinning is described in detail in DE 198 45 133 A1 whereto reference is explicitly made herein.

In the step 109 the measuring values of the scattered rays as produced by the rebinning are subjected to one-dimensional filtering with a factor which increases ramp-like as a function of the spatial frequency. To this end, each time successive values are taken into account in a direction parallel to the plane of rotation, that is, along a row of the virtual  
 5 detector. This filtering is carried out along each row of the virtual detector for all projection angles.

In other embodiments the rebinning could also be omitted. It is known that in that case the filtering must be modified because the detector unit is curved, for example in the form of an arc around the radiation source or around the axis of rotation.

10 The filtered measuring values are subsequently used for the reconstruction of the scatter intensity distribution in the examination zone by back projection.

The back projection is carried out in a volume which is defined by the vectors  $\bar{x}$ ,  $\bar{y}$  and  $\bar{q}$ , the unity vectors  $\bar{x}$  and  $\bar{y}$  being situated in the rotational plane and being oriented horizontally and vertically, respectively, whereas the wave vector transfer  $\bar{q}$  is  
 15 oriented parallel to the axis of rotation. In other embodiments two other, linearly independent vectors of the plane of rotation can be used instead of the vectors  $\bar{x}$  and  $\bar{y}$ . As has already been stated, the amount of the wave vector transfer  $\bar{q}$  is proportional to the product of the inverse wavelength  $\lambda$  of the scattered X-ray quanta and the sine of one half of the scatter angle  $\Theta$ :

$$20 \quad q = (1/\lambda)\sin(\Theta/2) \quad (1)$$

The scatter angle  $\Theta$  can be determined on the basis of the arrangement of the examination zone 15 irradiated by the fan beam 41 and the detector unit 16 as shown in Fig. 7. As opposed to known two-dimensional methods based on back projection, this Figure takes into account the real geometry in medical applications. For one or each detector  
 25 element  $D_i$  this gives rise to different scatter angles  $\Theta$  which are calculated in conformity with the following equation:

$$\Theta = \arctan(a/d) \quad (2)$$

Therein,  $d$  denotes the distance of a scatter center  $S_i$  and  $a$  denotes the distance between the detector element  $D_i$  and the foot 12 of the detector.

30 The detector  $D_i$  detects rays which have been scattered at the angles  $\Theta_1 < \Theta < \Theta_2$  in the examination zone 15 irradiated by the fan beam 41.

From the above two equations the following equation is obtained for small angles  $\Theta$

$$q \approx a/(2d\lambda) \quad (3)$$

The variation of the value of the wave vector transfer  $\bar{q}$  in dependence on the distance  $d$  between a scatter center and the foot of the detector thus has the shape of a hyperbola and hence is not linear (shown in Fig. 8). It follows therefrom that the originally linear path of the scattered rays in the  $(x,y,q)$  space is curved. The back projection thus takes place along rays curved in the form of a hyperbola.

In the step 111 a voxel  $V(x,y,q)$  is determined within a selectable  $(x,y)$  zone (field of view or FOV) and within a range of values of the wave vector transfer  $\bar{q}$  resulting from the geometry of the computer tomograph.

In the step 113 the filtered values are multiplied by a weighting factor which corresponds to the reciprocal value of the cosine of the scatter angle. The decreasing effective detector surface as a function of an increasing scatter angle is thus taken into account. When said angle is small, the cosine of the angle is practically always 1, so that this weighting can be dispensed with. Moreover, the fact that the radiation density decreases as the distance between the scatter center increases, that is, the voxel  $V(x,y,q)$ , and the point of incidence of the scattered ray on the measuring surface increases is taken into account by multiplying all measuring values for each radiation source position by a weighting factor which corresponds to the square of the distance between the scatter center, at which the ray associated with the measuring value was scattered, and the point of incidence of the scattered ray on the measuring surface.

When the rebinning is omitted in other versions, an additional multiplication of the filtered measuring values by a weighting factor is necessary; this factor is equal to the reciprocal value of the square of the distance between the radiation source position and the scatter center at which the detected ray was scattered.

During the back projection in the step 115 all curved rays are then taken into account which pass through the voxel  $V(x,y,q)$ . If not one ray from a radiation source position passes exactly through the center of the voxel, the associated value must be determined by interpolation of the measuring values of neighboring rays. The measuring value that can be associated with the ray passing through the voxel, or the measuring value obtained by interpolation, is accumulated on the voxel  $V(x,y,q)$ . After the contributions to the relevant voxel have thus been accumulated for all radiation source positions, it is checked in the step 117 whether all voxels in the  $(x,y,q)$  zone to be reconstructed have been dealt with. If this is not the case, the flow chart branches to the step 111. Otherwise the scatter intensity

distribution has been determined for all voxels in the FOV and the reconstruction method is terminated (step 119).

In other versions the back projection in the volume defined by two linearly independent vectors of the rotational plane and the wave vector transfer can be carried out as an approximation along straight rays.

5

## CLAIMS:

1. A computed tomography method comprising the steps of:
  - a) generating, using a radiation source (S) and a diaphragm arrangement (31) which is arranged between the examination zone (13) and the radiation source (S), a fan beam (41) which traverses an examination zone (13) or an object present therein,
  - 5 b) generating relative motions, comprising a rotation about an axis of rotation (14), between the radiation source (S) on the one side and the examination zone (13) or the object on the other side,
  - c) acquiring measuring values which are dependent on the intensity of the radiation by means of a detector unit (16) which detects, during the relative motions, the primary  
10 radiation from the fan beam (41) and radiation which is coherently scattered in the examination zone (13) or on the object,
  - d) reconstructing a CT image of the examination zone (13) from the measuring values, during which reconstruction a back projection is carried out in a volume which is defined by two linearly independent vectors of the rotational plane and a wave vector  
15 transfer.
2. A computed tomography method as claimed in claim 1, in which the back projection during the reconstruction step d) is performed along rays having a curved shape.
- 20 3. A computed tomography method as claimed in claim 1, in which prior to the back projection in the reconstruction step d) the measuring values are multiplied by a first weighting factor which corresponds to the square of the distance between the scatter center, at which the detected ray was scattered, and the point of incidence of the scattered ray on the detector unit, and by a second weighting factor which corresponds to the reciprocal value of  
25 the cosine of the scatter angle.
4. A computed tomography method as claimed in claim 3, in which prior to the back projection in the reconstruction step d) all measuring values for each radiation source position are multiplied by a weighting factor which corresponds to the reciprocal value of the

square of the distance between the radiation source position and the scatter center at which the detected ray was scattered.

5. A computed tomography method as claimed in claim 1, in which the

5 reconstruction step d) comprises the following steps:

- one-dimensional filtering of the measuring values in the direction parallel to the rotational plane,
- rebinning of the measuring values so as to form a number of groups, each measuring value measured by a detector element being associated with a line from the detector
- 10 element to the radiation source position and each group comprising a plurality of planes which are parallel to one another and to the axis of rotation and in which a respective line fan (411 ... 415) is situated,
- reconstruction of the distribution of the scatter intensity from the measuring values, a back projection then being carried out in a volume which is defined by two linearly
- 15 independent vectors of the rotational plane and a wave vector transfer.

6. A computer tomograph for carrying out the method claimed in claim 1, comprising

- a radiation source (S) and a diaphragm arrangement (31) which is arranged between
- 20 the examination zone (13) and the radiation source (S), in order to generate a fan beam (41) which traverses an examination zone (13) or an object present therein,
- a detector unit (16) which is coupled to the radiation source (S) and comprises a measuring surface (17),
- a drive arrangement (2, 5) for displacing an object present in the examination zone
- 25 (13) and the radiation source (S) relative to one another about an axis of rotation (14) and/or parallel to the axis of rotation (14),
- a reconstruction unit (10) for reconstructing the distribution of the scatter intensity within the examination zone from the measuring values acquired by the detector unit (16),
- 30 - a control unit (7) for controlling a radiation source (S), the detector unit (16), the drive arrangement (2, 5) and the reconstruction unit (10) in conformity with the steps a) to d) of claim 1.

7. A computer program for a control unit (7) for controlling a radiation source (S), a diaphragm arrangement (31), a detector unit (16), a drive arrangement (2, 5) and a reconstruction unit (10) of a computer tomograph so as to carry out the steps of claim 1.

1/6

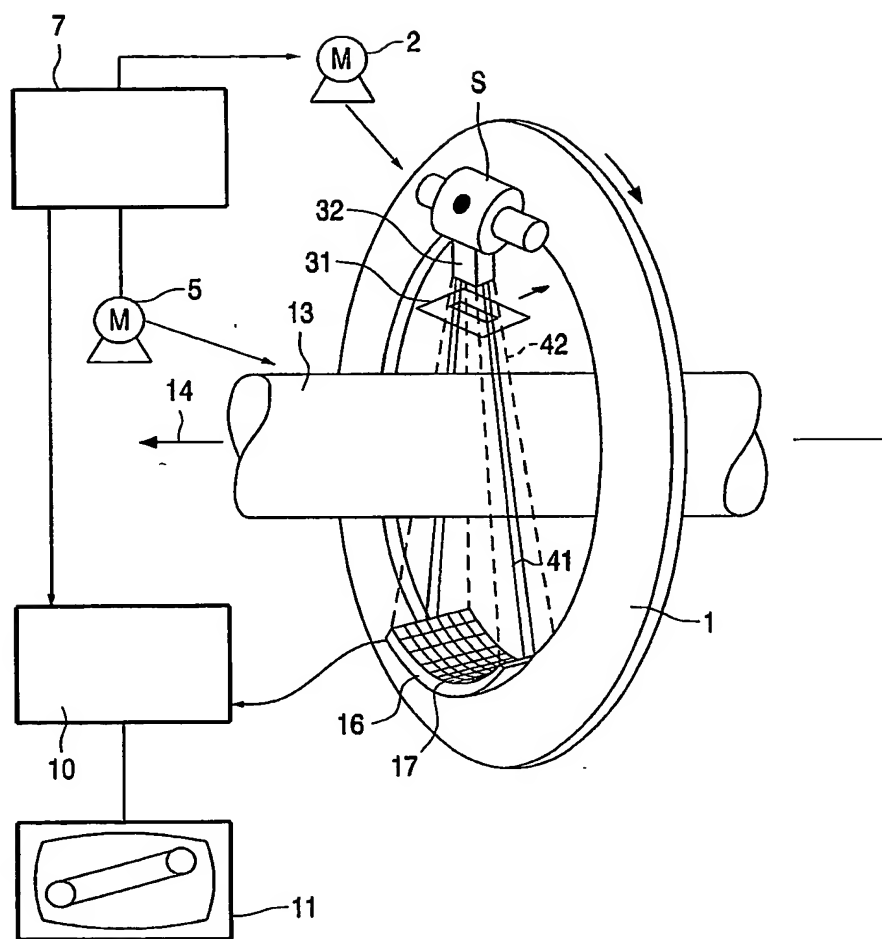


Fig.1



2/6

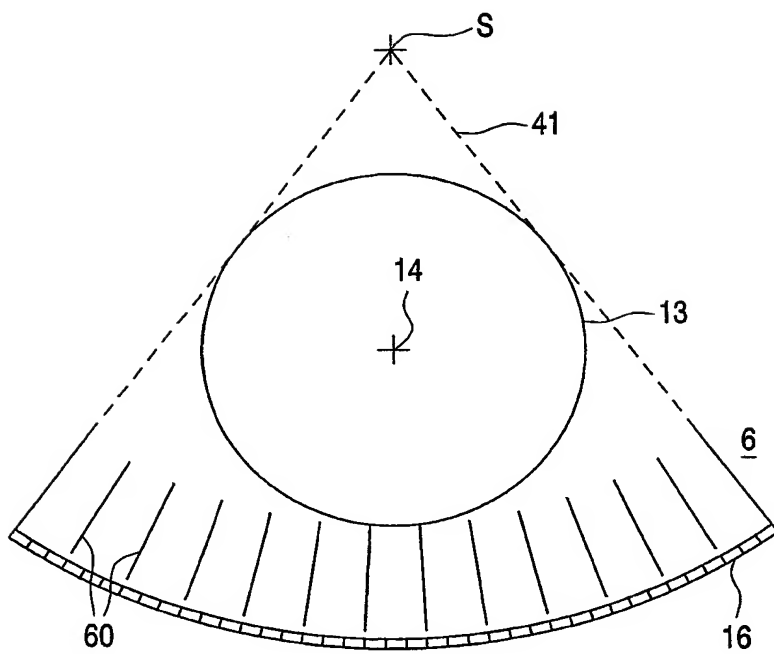


Fig.2

3/6

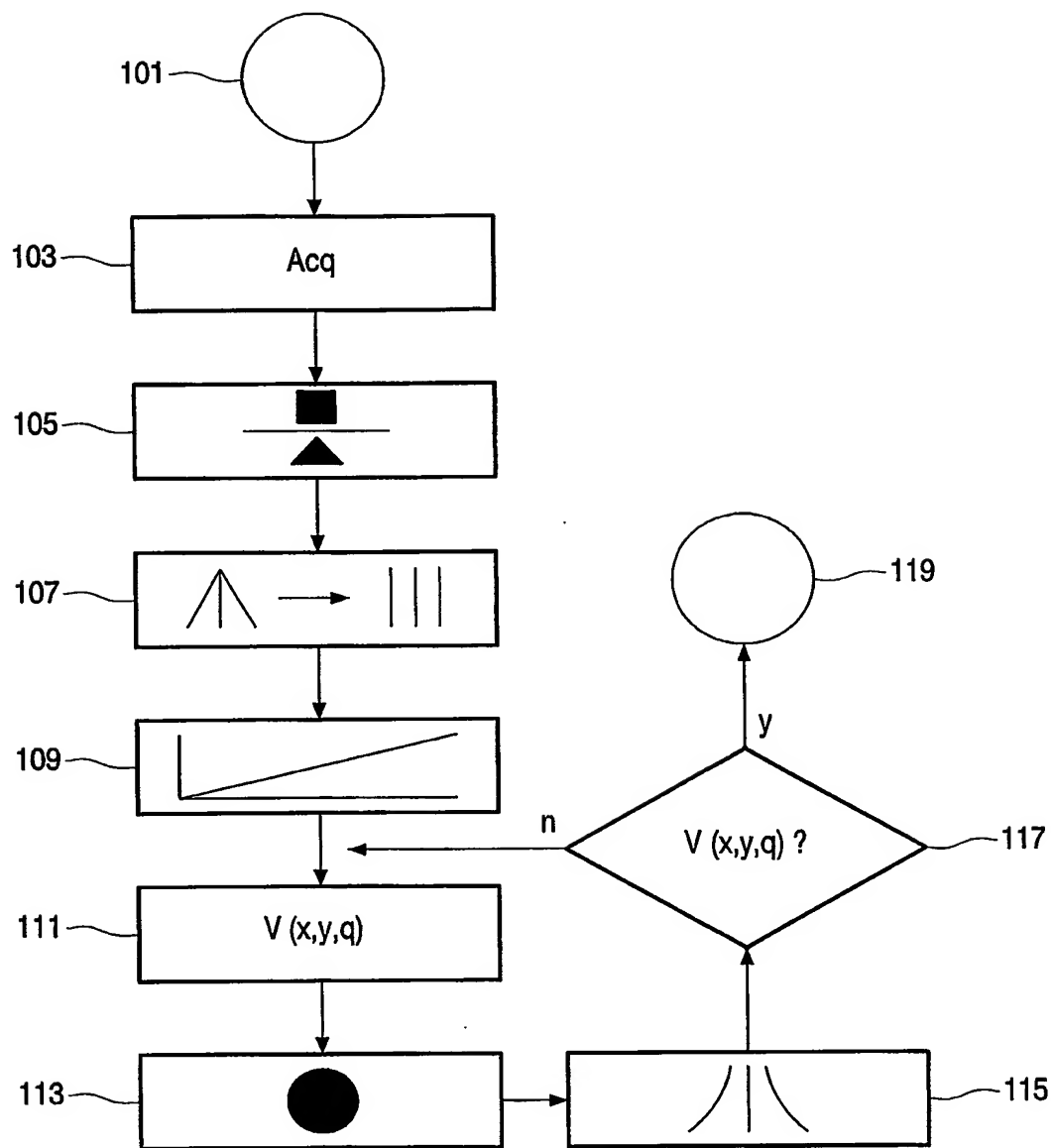


Fig.3

4/6

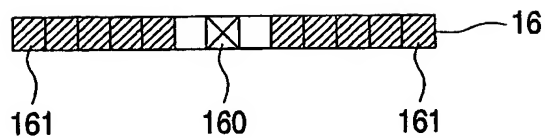


Fig.4

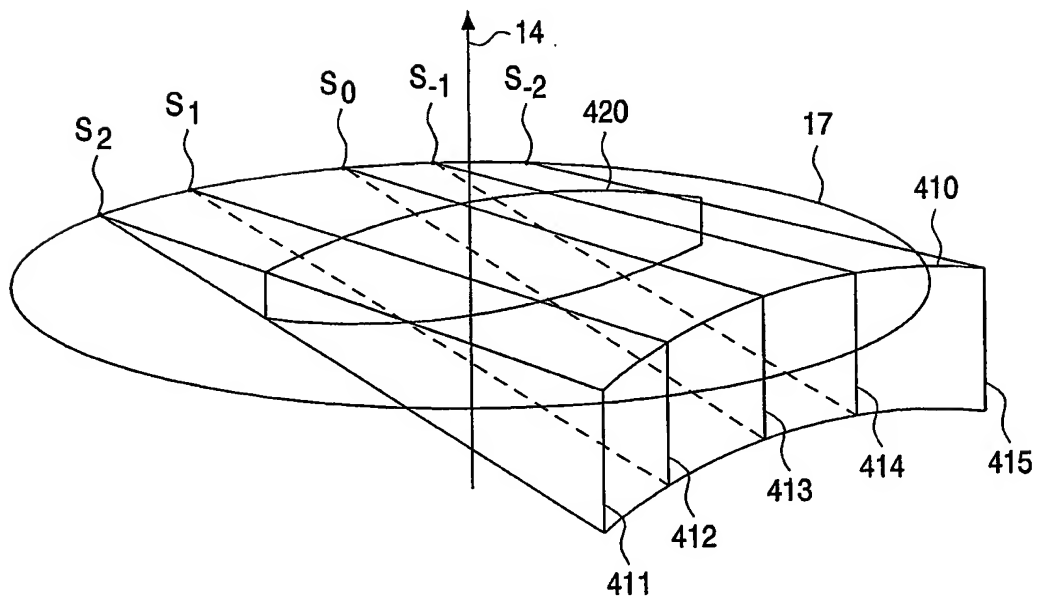


Fig.5

5/6

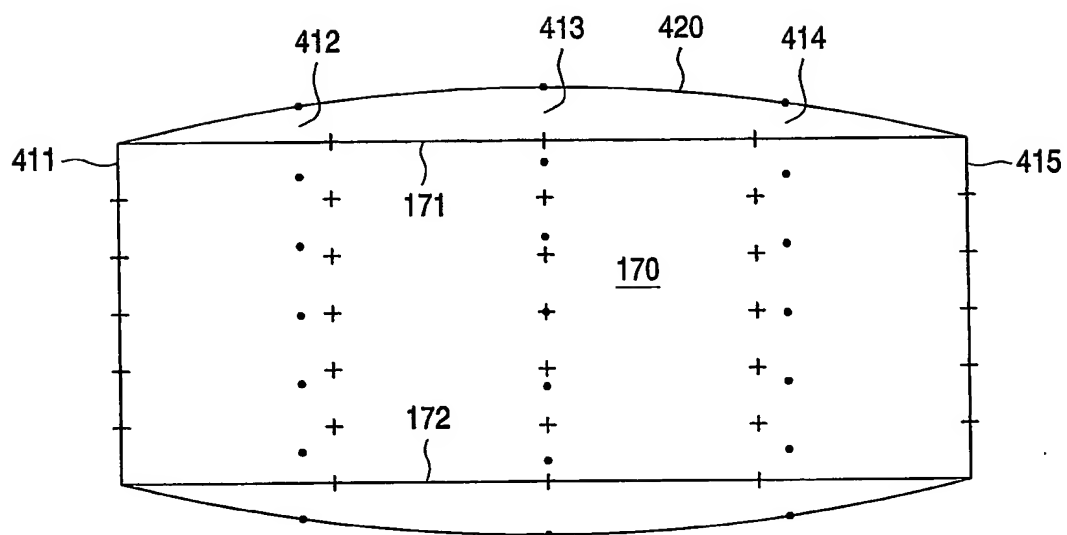


Fig.6

6/6

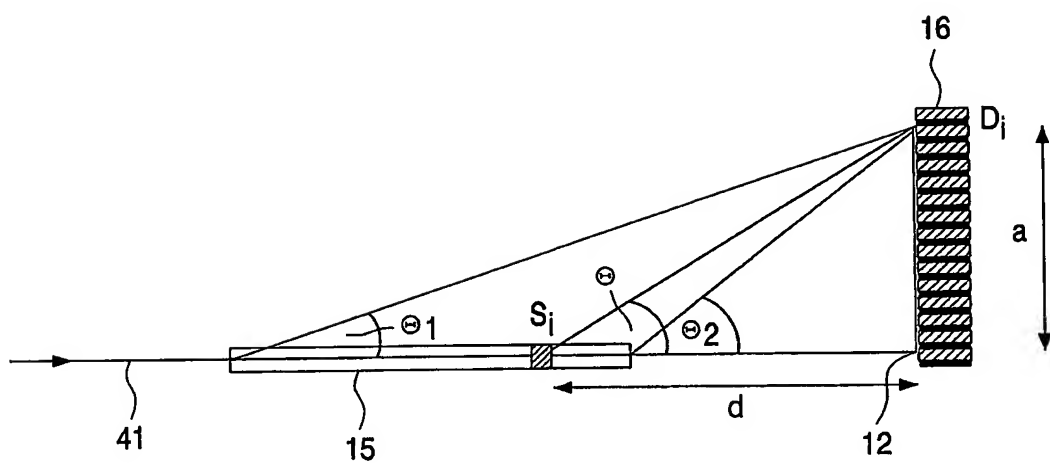


Fig.7

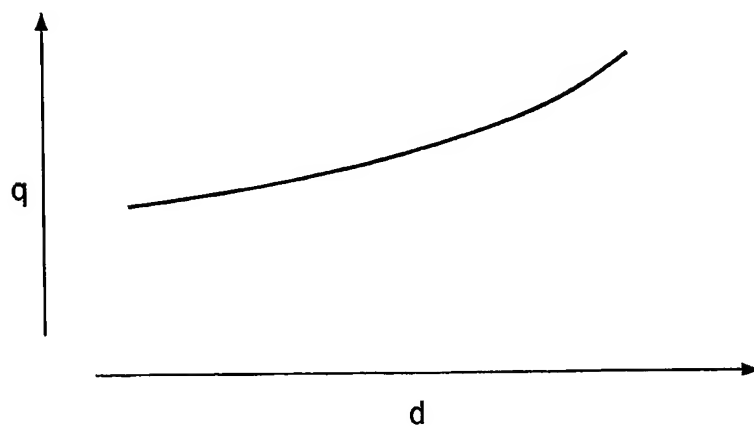


Fig.8

# INTERNATIONAL SEARCH REPORT

International Application No.  
PCT/IB 03/04749

A. CLASSIFICATION OF SUBJECT MATTER  
IPC 7 G06T11/00 A61B6/03

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
IPC 7 G06T A61B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	GRASS M ET AL: "3D CONE-BEAM CT RECONSTRUCTION FOR CIRCULAR TRAJECTORIES" PHYSICS IN MEDICINE AND BIOLOGY, TAYLOR AND FRANCIS LTD. LONDON, GB, vol. 45, no. 2, February 2000 (2000-02), pages 329-347, XP000993403 ISSN: 0031-9155 abstract; figures 1B-D,,9A,,11 page 330, paragraph 2 -page 333, paragraph 1 page 333, paragraphs 2,5	1,2,5-7
P,X	DE 102 15 890 A (PHILIPS INTELLECTUAL PROPERTY) 23 October 2003 (2003-10-23) abstract; figures 1-5 paragraphs '0019!', '0025!'-'0027!', '0030!'-'0044! --- -/--	1,2,5-7

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

### \* Special categories of cited documents:

- \*A\* document defining the general state of the art which is not considered to be of particular relevance
- \*E\* earlier document but published on or after the international filing date
- \*L\* document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- \*O\* document referring to an oral disclosure, use, exhibition or other means
- \*P\* document published prior to the international filing date but later than the priority date claimed

- \*T\* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- \*X\* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- \*Y\* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.
- \*&\* document member of the same patent family

Date of the actual completion of the international search

11 February 2004

Date of mailing of the international search report

19/02/2004

Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2  
NL - 2280 HV Rijswijk  
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,  
Fax: (+31-70) 340-3016

Authorized officer

Lahorte, P

# INTERNATIONAL SEARCH REPORT

International Application No  
PCT/IB 03/04749

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT		
Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
P,X	DE 101 59 927 A (SIEMENS AG) 26 June 2003 (2003-06-26) abstract; figures 1,3 paragraphs '0006!-'0013!,'0032!,'0041!-'0055! -----	1,2,5-7
X	US 6 285 733 B1 (GRASS MICHAEL ET AL) 4 September 2001 (2001-09-04) abstract; figures 1-6 column 1, line 59 -column 2, line 36 column 5, line 44 -column 6, line 35 column 7, line 15 -column 8, line 53 -----	1,2,5-7
X	US 2001/038678 A1 (GRASS MICHAEL ET AL) 8 November 2001 (2001-11-08) abstract; figures 1-3,5-7 paragraphs '0010!-'0014! paragraphs '0037!-'0047! paragraphs '0051!-'0056! -----	1,2,5-7

# INTERNATIONAL SEARCH REPORT

International Application No  
PCT/IB 03/04749

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
DE 10215890 A	23-10-2003	DE 10215890 A1 WO 03085390 A2	23-10-2003 16-10-2003
DE 10159927 A	26-06-2003	DE 10159927 A1 JP 2003180676 A US 2003133533 A1	26-06-2003 02-07-2003 17-07-2003
US 6285733 B1	04-09-2001	DE 19845133 A1 EP 0990892 A2 JP 2000107167 A	06-04-2000 05-04-2000 18-04-2000
US 2001038678 A1	08-11-2001	DE 10021219 A1 EP 1150251 A2 JP 2002045355 A	31-10-2001 31-10-2001 12-02-2002